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电动重卡替代柴油重卡的全生命周期碳减排效益分析

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摘要:为精准预测电动重卡替代柴油重卡的全生命周期碳减排效益,以单辆重卡为对象,通过预测2023~2050年的电力和柴油 碳排放因子变化特性,耦合两类重卡寿命及生命周期行驶里程,分阶段构建了重卡动态碳排放模型,深入分析了"2050年净 零排放(NZE)情景"、"承诺目标(APS)情景"和"既定政策(STEPS)情景"下两类重卡的碳排放足迹,并计算碳减排量和碳减 排率.结果表明,电池生产和电池回收是分别导致电动重卡生产阶段和拆解回收阶段碳减排效益不佳的重要因素.电力碳排放 因子(以CO2计)每降低1g·(kW·h)⁻¹,电动重卡全生命周期碳排放可减少1.74t.3种情景下,两类重卡运行阶段碳排放均占全 生命周期碳排放总量的90%以上.碳减排效益由高到低的情景依次为NZE、APS和STEPS,其对应的全生命周期碳减排量分别 为1054.68、1021.78和1007.97t,碳减排率分别为54.38%、52.68%和51.97%.

关键词:重卡;碳排放因子;动态模型;情景分析;碳排放;全生命周期

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Life Cycle Carbon Reduction Benefits of Electric Heavy-duty Truck to Replace Diesel **Heavy-duty Truck**

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Abstract: To accurately predict the life-cycle carbon reduction benefits of replacing a diesel heavy-duty truck with an electric one, taking a single heavy-duty truck as the object, the variation trend in electric and diesel carbon emission factors from 2023 to 2050 were predicted; coupled with the life spans and life-cycle mileage of the two types of heavy-duty trucks, a dynamic carbon emission model for the heavy-duty trucks was constructed in stages. The carbon footprints of the trucks under the "Net Zero Emissions by 2050 Scenario (NZE)", "Announced Pledges Scenario (APS)", and "Stated Policies Scenario (STEPS)" were analyzed. In addition, the carbon reduction and carbon reduction rate were calculated. The results showed that battery manufacturing and battery recycling were the main factors to impair the improvement of carbon reduction in the production and recycling stages of electric heavy-duty trucks, respectively. For every 1 g (kW h)⁻¹ reduction in the electricity carbon emission factor (CO₂), an electric heavy-duty truck could reduce 1,74 t of carbon emissions over its life cycle. Under the three scenarios, the carbon emissions during the operation stage of both types of heavy trucks accounted for more than 90% of the total life-cycle carbon emissions. Carbon reduction benefits from the highest to the lowest were NZE, APS, and STEPS, and their corresponding life-cycle carbon emission reductions were 1054, 68, 1021. 78, and 1007. 97 t, with carbon reduction rates of 54. 38%, 52. 68%, and 51. 97%, respectively.

Key words: heavy-duty truck; carbon emission factor; dynamic model; scenario analysis; carbon emission; life cycle

交通运输碳排放量约占我国碳排放总量的 10%,是CO₂排放量增长最快的行业^[1,2],降碳可助 力实现《巴黎协定》及中国"双碳"目标[3~5].在温 室气体排放增幅最大的子行业——公路货运中,重 卡排放占整个交通运输碳排放总量的40%,重卡脱 碳是影响气候变化方面的当务之急[6~8].然而中国却 面临着重型运输减排难题, 电能替代有望成为其突 破降碳瓶颈进而推动运输行业深度脱碳的关键[9-11]. 系统评估电动重卡与柴油重卡碳排放,对挖掘电动 重卡减排潜力意义重大.

目前车辆碳排放大都聚焦于乘用车,重卡领域 关注较少.已有重卡碳排放研究多通过划定燃料边 界建立燃料生命周期或应用美国阿贡GREET模型对 电动重卡与柴油重卡碳排放进行评估[12~16],较少考 虑车辆生产与回收产生的碳排放.划定车辆生命周 期边界进而建立车辆生命周期可弥补以上不足,以 便对两类重卡碳排放进行更为精确的衡量[9,11,17,18].

但相关研究缺少整体考虑,未系统地对碳排放进行 阶段划分,同时欠缺电动重卡碳减排效益直观表 征.此外,借助敏感性分析可更为深入地探究重卡 碳排放^[7,8,11,14,17],通过重卡技术、中国碳减排政策 与电动车辆所占比例等设置情景能预测未来电动重 卡对气候影响[6.7.13,15,19,20]. 但已有研究总体上对电动 重卡碳减排效益定性讨论及预测考虑不够全面,多 局限于固定年份的能源碳排放因子评估重卡全生命 周期碳排放,忽略了重卡运行年限期间电力及柴油 碳排放因子随时间变化所带来的影响,缺乏生命周 期碳排放足迹追踪.

基于此,本文按生命线对电动重卡与柴油重卡

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(4)

进行生命周期碳排放阶段划分,综合考虑未来电 力、柴油碳排放因子变化和重卡车辆特性,构建两 类重卡动态碳排放模型,引入"2050年净零排放 (NZE)情景"、"承诺目标(APS)情景"和"既定政 策(STEPS)情景"分析两类重卡全生命周期碳排放 足迹,并计算碳减排量和碳减排率.

1 材料与方法

1.1 全生命周期碳排放分析框架

重卡生命周期碳排放与汽车类似,边界为制造 开始到使用结束^[21],本文按生命线将其分为生产、 运行与拆解回收这3个阶段.设定生产阶段边界为车 辆零配件的生产到整车形成;运行阶段边界为车辆 出厂到报废结束;拆解回收阶段为报废结束到车辆 拆解完成.划分结果如图1所示.



1.2 能源碳排放因子预测模型构建

PMF法广泛应用于土壤重金属源解析、PM₂₅来 源定量分析等领域^[22,23],是一种将污染源贡献与污 染源组分联系起来的新方法^[24].本研究参考 PMF法 并以唐一媛等^[25]建立的模型为基础,结合国际能源 署(IEA)对发展中国家的电力需求预测,引入主要 的6类发电方式年增长率重构了电力碳排放因子动 态模型.Zhang等^[11]预测柴油机碳排放每5a减少3%. 而柴油机碳排放主要来自柴油燃烧,因此可将其产 生的碳减排转移至柴油,即柴油机的碳减排间接降 低了柴油碳排放因子.本研究取年减排率建立未来 柴油碳排放因子.本研究取年减排率建立未来 柴油碳排放因子动态预测模型.以y为基准年,n为 目标年的电力碳排放因子测算模型与柴油碳排放因 子测算模型,分别如式(1)和式(2)所示.

$$C_{ep,n} = \sum_{i=1}^{6} \frac{M_{i,y} (1 + \alpha_{i,n})^{n-y}}{\sum_{i=1}^{6} M_{i,y} (1 + \alpha_{i,n})^{n-y}} \cdot C_i$$
(1)

$$C_{dp,n} = C_{dp,y} (1 - \omega)^{n-y}$$
 (2)

式中, $C_{ep,n}$ 为目标年n电力碳排放因子[以CO₂计, kg·(kW·h)⁻¹]; $M_{i,y}$ 为基准年y的第i类发电方式发电 量(kW·h); $\alpha_{i,n}$ 为目标年n第i种发电方式的年发电 量增长率; C_i 为第i种发电方式的全生命周期碳排放 因子[以CO₂计, kg·(kW·h)⁻¹]; $C_{dp. n}$ 为目标年n的 柴油碳排放因子(以CO₂计, kg·L⁻¹); $C_{dp. y}$ 为基准年 y的柴油碳排放因子(以CO₂计, kg·L⁻¹), ω 为柴油 年均减排率.

1.3 碳排放模型构建

吨位接近的电动重卡与柴油重卡载重量相差不 大,故本文不考虑载重量对其碳排放影响,对各阶 段碳排放进行建模.

1.3.1 生产阶段碳排放模型

基于重卡生命周期边界,重卡在生产过程中的 碳排放随各零配件比例波动而变化.将零配件在生 产过程中的温室气体排放纳入重卡生产阶段碳排 放,定义了柴油重卡与电动重卡生产阶段碳排放模 型,其中电动重卡生产阶段碳排放包括车辆及电池 制造,计算如式(3)和式(4)所示.

柴油重卡生产阶段碳排放模型:

 $E_{dhtb} = \sum M_{d} K_{id} C_{id}$ (3) 式中, E_{dhtb} 为柴油重卡生产阶段碳排放量(t); M_{d} 为柴油重卡质量(t); K_{id} 为柴油重卡第*i*种零配件占重 卡质量比例; C_{id} 为柴油重卡第*i*种零配件在生产时 的碳排放因子(以CO₂计, t·t⁻¹).

电动重卡生产阶段碳排放模型:

式中, E_{ehb} 为电动重卡生产阶段碳排放量(t); E_b 为电 池制造所产生的碳排放(t); E_{ehv} 为电动重卡车辆生产 时产生的碳排放(t); B_{ht} 为电池的容量(kW·h), C_{hbb} 为电池单位容量在制造时产生的碳排放量[以 CO₂计, t·(kW·h)⁻¹]; M_e 为电动重卡车辆质量(t); K_{ie} 为电动 重卡第*i*种零配件占重卡质量比例; C_ie 为电动重卡第 *i*种零配件在生产时的碳排放因子(以 CO₂计, t·t⁻¹). **1.3.2** 运行阶段年碳排放模型

运行阶段电动重卡将碳排放转移至能源上游 (发电侧)^[26],其碳排放对电力碳排放因子变动有着 极强的敏感性.综合考虑充电损耗^[27]、电厂内耗与 电能输送损失产生的影响,引用边际发电量因子 (PMP)^[28]建立电动重卡运行阶段的动态年碳排放模 型.而柴油重卡运行阶段碳排放主要来自柴油燃烧, 故结合行驶里程及柴油碳排放因子建立动态年碳排 放模型^[29].两类重卡运行阶段的动态年碳排放模型 如式(5)和式(6)所示.

柴油重卡运行阶段年碳排放模型:

$$E_{\rm dhto, n} = \frac{L_{\rm d, n} \cdot D_{\rm ad} \cdot C_{\rm dp, n}}{100 \times 1\,000}$$
(5)

式中, $E_{\text{dhto},n}$ 为n年柴油重卡运行阶段的年 CO_2 排放量(t); $L_{\text{d},n}$ 为n年柴油重卡年运行里程(km); D_{ad} 为

柴油重卡油耗[L·(100 km)⁻¹]; *C*_{dp,n}为n年柴油碳排 放因子(以CO₂计, kg·L⁻¹).

电动重卡运行阶段年碳排放模型:

$$E_{ehto, n} = \frac{L_{e, n} \cdot D_{ae} \cdot C_{ep, n} \cdot PMP_{1}}{100 \times 1000}$$
(6)

其中: PMP₁ = $\frac{1}{\eta \cdot (1 - LR) \cdot (1 - PR)}$

式中, $E_{ehto,n}$ 为n年电动重卡运行阶段的年 CO₂排放 量(t); $L_{e,n}$ 为n年电动重卡年运行里程(km); D_{ae} 为 电动重卡百公里电耗[kW·h·(100 km)⁻¹]; $C_{ep,n}$ 为n年电力碳排放因子[以CO₂计,kg·(kW·h)⁻¹];PMP₁ 为充电边际发电量因子,即电动重卡充电1 kW·h引 起发电侧的发电增量值; η 为电动重卡充电效率; LR为线损率;PR为厂用电率.

1.3.3 拆解回收阶段碳排放模型

资源循环利用是节能降碳的一个重要途径,重 卡回收可降低制造阶段的能源消耗及温室气体排 放^[30].有研究发现^[31,32],柴油卡车发动机与电动卡车 电机的差异是导致两类卡车铸铁与铜含量不同的主 要因素,故本文将其视为柴油重卡与电动重卡车辆 的重要组成部分,并假设二者在拆解回收阶段的碳 排放无显著差异^{(33]},即两类重卡在拆解回收阶段的 碳排放差异主要取决于车辆和电池,且整车在拆解 回收阶段只消耗电能^[20].定义了拆解回收阶段动态 碳排放模型如式(7)和式(8)所示.

柴油重卡拆解回收阶段碳排放模型: $E_{dbtr,n} = 0.277 \cdot W_{dsr} \cdot M_{d} \cdot PMP_2 \cdot C_{ep,n}$ 其中: PMP_2 = $\frac{1}{(1 - LR) \cdot (1 - PR)}$

式中, $E_{dhr,n}$ 为n年柴油重卡拆解回收阶段产生的碳 排放量(t); W_{dsr} 为每千克柴油重卡拆解回收阶段消 耗的能量(MJ·kg⁻¹);PMP₂为用电边际发电量因子, 是拆解与回收重卡车辆每消耗1kW·h电量引起的发 电侧的发电增量值.

电动重卡拆解回收阶段碳排放模型:

 $E_{ehtr,n} = 0.277 8 \cdot (W_b M_b + W_{esr} M_e) \cdot PMP_2 \cdot C_{ep,n}$ (8) 式中, $E_{ehtr,n} \partial n$ 年电动重卡拆解回收阶段产生的碳 排放量(t); W_b 为电动重卡电池拆解回收阶段耗能 (MJ·kg⁻¹); M_b 为电动重卡电池质量(t); W_{esr} 为回收 1 kg电动重卡车辆所需要的能量(MJ·kg⁻¹).

1.3.4 全生命周期碳排放模型

电动重卡运行阶段和拆解回收阶段碳排放与电 力碳排放因子密切相关,而柴油碳排放因子对柴油 重卡运行阶段排放有着重大影响.基于电力碳排放 因子逐年随电力结构变化,以及柴油机效率提高和 排气后处理系统技术发展,柴油碳排放因子间接逐 年降低,考虑到重卡寿命及生命总里程数变化不 大,得出其总排放与两类重卡购入年限、年运行情 况和重卡寿命相关.本文提出一种与运行里程相关 联的重卡全生命周期碳排放模型,如式(9)~(14)所 示.为方便分析,模型假设:①两类重卡购入时间 为X年,且均为年初,即当年的1月1日;②每种情 景下年运行里程不变,相同情景下两类重卡实际年 运行里程 $L_{d,a}$ 和 $L_{e,a}$ 相同;③柴油重卡与电动重卡的 生命周期行驶里程分别为 L_{d} 和 L_{e} ;④柴油重卡寿命 为 S_{d} ,电动重卡寿命为 S_{e} ;⑤对应情景下柴油重卡 与电动重卡理论总运行年限分别为 $\gamma_{d} = L_{d}/L_{d,a}$ 和 $\gamma_{e} = L_{e}/L_{e,a}$;⑥总运行里程达重卡生命周期行驶里程或 理论总运行年限达重卡寿命,重卡即报废.

柴油重卡全生命周期碳排放模型:

① $\gamma_d < S_d$ $E_{td} = E_{dhtb} + E_{dhto} + E_{dhtr, X + R_d(\gamma_d)} = E_{dhtb} + \sum_{i=x}^{X + R_d(\gamma_d)^{-1}} E_{dhto,i} + E_{dhto,X + R_d(\gamma_d)} + E_{dhtr,X + R_d(\gamma_d)}(9)$ 其中: $E_{dhto,X + R_d(\gamma_d)} = \frac{\left[L_d - L_{d,a} \cdot R_d(\gamma_d)\right] \cdot D_{ad} \cdot C_{dp,X + R_d(\gamma_d)}}{100 \times 1000}$ 式中, E_{id} 为柴油重卡全生命周期碳排放(t); E_{dhto} 为 柴油重卡运行阶段总碳排放(t); $R_d()$ 为向下取整函 数; $E_{dhtr,X + R_d(\gamma_d)}$ 为 $X + R_d(\gamma_d)$ 年柴油重卡拆解回收产生 的碳排放(t); $E_{dhto,i}$ 为i年柴油重卡年运行碳排放(t); $E_{dhto,X + R_d(\gamma_d)}$ 为 $X + R_d(\gamma_d)$ 年柴油重卡年运行碳排放(t); $E_{dhto,X + R_d(\gamma_d)}$ 为 $X + R_d(\gamma_d)$ 年 的柴油 酸排放因子(以CO₂ 计, kg·L⁻¹).

$$(2)\gamma_{d} = S_{d}$$

$$E_{td} = E_{dhtb} + E_{dhto} + E_{dhtr, X + R_{d}(S_{d})} = E_{dhtb} + \sum_{i=X}^{X + R_{d}(S_{d})^{-1}} E_{dhto, i} + E_{dhto, X + R_{d}(S_{d})} + E_{dhtr, X + R_{d}(S_{d})}$$

$$(10)$$

其中:

$$E_{\text{dhto}, X + R_{a}(S_{d})} = \frac{\left[L_{d} - L_{d,n} \cdot R_{d}(S_{d})\right] \cdot D_{\text{ad}} \cdot C_{\text{dp}, X + R_{a}(S_{d})}}{100 \times 1\ 000}$$

式中, $E_{dhtr, X + R_{d}(S_{d})}$ 为 $X + R_{d}(S_{d})$ 年柴油重卡拆解回收产 生的碳排放(t); $E_{dhtr, X + R_{d}(S_{d})}$ 为 $X + R_{d}(S_{d})$ 年柴油重卡年 运行碳排放(t); $C_{dp, X + R_{d}(S_{d})}$ 为 $X + R_{d}(S_{d})$ 年的柴油碳排 放因子(以 CO₂计, kg·L⁻¹).

$$(3) \gamma_{d} > S_{d}$$

$$E_{td} = E_{dhtb} + E_{dhto} + E_{dhtr, X + R_{d}(S_{d})} = E_{dhtb} + \sum_{i=X}^{X + R_{d}(S_{d})^{-1}} E_{dhto, i} + E_{dhto, X + R_{d}(S_{d})} + E_{dhtr, X + R_{d}(S_{d})}$$

$$(11)$$

其中:

$$E_{\text{dhto},X+R_{d}}(S_{d}) = \frac{\left[S_{d} - R_{d}(S_{d})\right] \cdot L_{d,n} \cdot D_{ad} \cdot C_{dp,X+R_{d}}(S_{d})}{100 \times 1000}$$

$$\oplus \overline{a} \overline{b} \overline{a} \overline{b} \overline{c} \underline{c} \underline{c} \overline{c} \overline{b} \overline{a} \overline{b} \overline{b} \overline{b} \overline{b} \overline{b} \overline{b} \overline{c} \overline{b} \overline{c} \overline{c} \overline{c} \overline{c}$$

$$\overline{U} \gamma_{e} < S_{e}$$

$$E_{te} = E_{ehtb} + E_{ehto} + E_{ehtr,X+R_{d}}(\gamma_{e}) = E_{ehtb} + \sum_{i=X}^{X+R_{d}} \sum_{i=X}^{R_{d}} E_{ehto,i} + E_{ehto,X+R_{d}}(\gamma_{e}) + E_{ehtr,X+R_{d}}(\gamma_{e})$$

$$(12)$$

其中:

$$E_{\text{ehto}, X + R_{d}(\gamma_{e})} = \frac{\left[L_{e} - L_{e,n} \cdot R_{d}(\gamma_{e})\right] \cdot D_{ae} \cdot C_{ep, X + R_{d}(\gamma_{e})} \cdot PMP_{1}}{100 \times 1000}$$

式中, E_{le} 为电动重卡全生命周期碳排放(t); E_{ehto} 为 电动重卡运行阶段总碳排放(t); $E_{ehtr,X+R_{d}(\gamma_{e})}$ 为X+ $R_{d}(\gamma_{e})$ 年电动重卡拆解回收产生的碳排放(t); $E_{ehto,i}$ 为*i*年电动重卡年运行碳排放(t); $E_{ehto,X+R_{d}(\gamma_{e})}$ 为X+ $R_{d}(\gamma_{e})$ 年电动重卡年运行碳排放(t); $C_{ep,X+R_{d}(\gamma_{e})}$ 为 X+ $R_{d}(\gamma_{e})$ 年的电力碳排放因子[以CO₂计, kg·(kW·h)⁻¹].

$$(2) \gamma_{e} = S_{e}$$

$$E_{te} = E_{ehtb} + E_{chto} + E_{ehtr, X + R_{d}(S_{e})} = E_{ehtb} +$$

$$\sum_{i=X}^{X + R_{d}(S_{e}) + 1} E_{ehto, i} + E_{ehto, X + R_{d}(S_{e})} + E_{ehtr, X + R_{d}(S_{e})}$$

$$(13)$$

$$\downarrow \psi :$$

$$E_{ehto, X + R_{d}(S_{e})} =$$

$$\underbrace{ \left[L_{e} - L_{e,a} \cdot R_{d}(S_{e}) \right] \cdot D_{ae} \cdot C_{ep, X + R_{d}(S_{e})} \cdot PMP_{1} }_{100 \times 1\ 000}$$

式中, $E_{ehtr,X+R_{d}(S_{e})}$ 为 $X+R_{d}(S_{e})$ 年电动重卡拆解回收产 生的碳排放(t); $E_{ehto,X+R_{d}(S_{e})}$ 为 $X+R_{d}(S_{e})$ 年电动重卡 年运行碳排放(t); $C_{ep,X+R_{d}(S_{e})}$ 为 $X+R_{d}(S_{e})$ 年的电力碳

排放因子[以 CO₂计, kg·(kW·h)⁻¹].
③
$$\gamma_e > S_e$$

 $E_{te} = E_{ehtb} + E_{ehto} + E_{ehtr, X + R_d(S_e)} = E_{ehtb} + \sum_{i=X}^{X + R_d(\gamma_e)^{-1}} E_{ehto,i} + E_{ehto, X + R_d(S_e)} + E_{ehtr, X + R_d(S_e)}$
(14)
其中:
 $E_{ehto, X + R_d(S_e)} = [S_e - R_d(S_e)] \cdot L_{e,n} \cdot D_{ae} \cdot C_{ep, X + R_d(S_e)} \cdot PMP_1$

 100×1000

1.3.5 碳减排量及碳减排率模型

为直观比较两类重卡的全生命周期碳排放,引 入碳减排量与碳减排率^[34]表征电动重卡替代柴油重 卡的碳减排效益.假设柴油重卡实际总运行L_{da}公里, 电动重卡实际共运行L_{ea}公里,碳减排量及碳减排率 可通过式(15)和式(16)获得.

碳减排量模型:~



应用姜运哲等^[35]所提及的短道运输,选用电厂 到煤矿的短途运输作为研究场景.结合2021年电动 重卡销量,选择销量第一的汉马科技之华菱之星6 ×4换电式纯电动牵引车作为研究对象,并以其生产 的华菱汉马H7重卡450 PS,6×4牵引车进行对比. 本文重卡车辆相关数据来源于贵州某电厂,该电厂 提供的重卡参数如表1所示.

	表1	重卡参数	
Table 1	Heavy	-dutv truck	parameters

会料 4 4	车辆类型					
豕 奴名称 —	电动重卡	柴油重卡				
车辆型号	汉马科技之华菱之星6×4换电式纯 电动牵引车HN4253H36C8BEV	华菱汉马H7重卡450 PS,6×4牵引车 HN4252H46C4MS				
平均百公里油耗/L	—	60				
平均百公里电耗/kW·h	170	—				
平均车辆整备质量/t	11	8.5				
载重量/t	30	32				
电池重量/t	2.98	—				
电池容量/kW·h	282	—				
充电效率/%	90	_				

1.4.2 碳排放清单构建

本文假设无论电池的化学成分或充电容量如

何,电池寿命与车辆寿命相当^[36].2021年全国线损 率为5.26%,厂用电率为4.36%^[37],柴油排放量每5 a降低3%^[11].重卡在生产阶段与拆解回收阶段的相 关参数如表2所示.

各发电方式的碳排放因子[25]如表3所示,本文 假定未来除煤电外,其它发电方式碳排放因子波动 不大.

制造重卡使用材料的组成比例和该材料在生产 过程中所产生的碳排放将直接影响整个生产阶段的 碳排放总量,因此需将整车制造过程中各材料占比

以及各材料在生产过程的碳排放整合成一个整体框 架.由文献[20,34]可知,电动重卡与柴油重卡在 生产过程中所需材料(不含电池)成分比例及各材料 制造过程中所产生的碳排放如表4所示.

1.4.3 发电量及电力结构

国际能源署(IEA)^[39,40]对中国 2021、2030 和 2050年的电力结构和发电量统计与预测如表5 所示.

	表 2	碳	排放清单	<u>á</u>
Table 2	Carl	oon	emission	inventory

参数名称 重卡类型 电动重卡 电动重卡 柴油重卡 电池制造碳排放(以 CO ₂ 计) ^[21] /t·(kW·h) ⁻¹ 0.10 - 柴油生命周期碳排放因子(以 CO ₂ 计) ^{116]} /kg·L ⁻¹ - 3.96 全国电力碳排放因子(以 CO ₂ 计) ^{137]} /kg·(kW·h) ⁻¹ 0.56 - 车身回收耗能 ^[38] /MJ·kg ⁻¹ 0.37 0.37 电池拆解回收耗能 ^[38] /MJ·kg ⁻¹ 31 -			
电动重卡 电动重卡 柴油重卡 电池制造碳排放(以CO ₂ 计) ^[21] /t·(kW·h) ⁻¹ 0.10 - 柴油生命周期碳排放因子(以CO ₂ 计) ^[16] /kg·L ⁻¹ - 3.96 全国电力碳排放因子(以CO ₂ 计) ^[37] /kg·(kW·h) ⁻¹ 0.56 - 车身回收耗能 ^[38] /MJ·kg ⁻¹ 0.37 0.37 电池拆解回收耗能 ^[38] /MJ·kg ⁻¹ 31 - 今件 会行咖 用用 ^[20] /um 820,000 700,000	<i>全粘力</i>	重卡类型	
电池制造碳排放(以 CO ₂ 计) ^[21] /t·(kW·h) ⁻¹ 0.10 - 柴油生命周期碳排放因子(以 CO ₂ 计) ^[16] /kg·L ⁻¹ - 3.96 全国电力碳排放因子(以 CO ₂ 计) ^[37] /kg·(kW·h) ⁻¹ 0.56 - 车身回收耗能 ^[38] /MJ·kg ⁻¹ 0.37 0.37 电池拆解回收耗能 ^[38] /MJ·kg ⁻¹ 31 - 今件, 令任, 命任, 即思見 ^[20] /dm 820,000 700,000	参姒石协 -	电动重卡	柴油重卡
柴油生命周期碳排放因子(以CO ₂ 计) ¹¹⁶ /kg·L ⁻¹ - 3.96 全国电力碳排放因子(以CO ₂ 计) ¹³⁷ /kg·(kW·h) ⁻¹ 0.56 - 车身回收耗能 ¹³⁸ /MJ·kg ⁻¹ 0.37 0.37 电池拆解回收耗能 ¹³⁸ /MJ·kg ⁻¹ 31 - 今件, 令任, 命任, 即田和 ¹²⁰ /um 820,000 700,000	电池制造碳排放(以CO ₂ 计) ^[21] /t·(kW·h) ⁻¹	0.10	—
全国电力碳排放因子(以CO ₂ 计) ^[37] /kg·(kW·h) ⁻¹ 0.56 - 车身回收耗能 ^[38] /MJ·kg ⁻¹ 0.37 0.37 电池拆解回收耗能 ^[38] /MJ·kg ⁻¹ 31 - 今件令行咖里用 ^[20] /um 820,000 700,000	柴油生命周期碳排放因子(以CO2计) ^[16] /kg·L ⁻¹	_	3.96
车身回收耗能 ^[38] /MJ·kg ⁻¹ 0.37 电池拆解回收耗能 ^[38] /MJ·kg ⁻¹ 31 今件令行咖里用 ^[20] /mm 820,000	全国电力碳排放因子(以CO ₂ 计) ^[37] /kg·(kW·h) ⁻¹	0.56	—
电池拆解回收耗能 ¹³⁸ /MJ·kg ⁻¹ 31 一	车身回收耗能 ^[38] /MJ·kg ⁻¹	0.37	0.37
<u> </u>	电池拆解回收耗能 ^[38] /MJ·kg ⁻¹	31	—
至至即11改至程 /Km 820 000 700 000	全生命行驶里程 ^[20] /km	820 000	700 000
使用寿命 ^[20] /a 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	使用寿命 ^[20] /a	8	(TAB

Table 5 Carbon emission is	actors for various power generation methods
发电方式	碳排放因子(以CO ₂ 计)/g·(kW·h) ⁻¹
太阳能光伏	94.80
风能	9.47
核能	3.37
天然气	412.78
煤炭	838.60
水电 1/1 0	22.20
2 结果与分析	F Sall
10 PM	AT I

表3 不同发电方式碳排放因子

情景分析广泛应用于污染物未来排放趋势预 测,通过设置多种发展情景,可预测不同情景下碳 排放[41, 42]. 本文聚焦近年来国际国内环境新形势, 借鉴国际能源署(IEA)^[39, 40]设立的3种电力发展情

景,选取2021年为基准年,同时以2030年和2050 年为目标年,采用情景分析法对电动重卡与柴油重 卡碳排放足迹进行研究.

2.1 情景设定

(1) 2050年净零排放(NZE)情景 为将全球温 升控制在1.5°C的目标,需在2050年实现净零排放. 可再生能源2030年发电量将占总发电量的60%以 上,到2050年,可再生能源发电量将占总发电量的 88%. 化石燃料的发电量则将在 2030年比 2021年减 少一半以上,到2050年则降为零.

(2) 承诺目标(APS)情景 假设各国政府的所 有气候承诺按时履行.可再生能源发电量将从2021 年占总发电量的28%增加到2030年的49%,并在 表4 重卡车辆材料分布及材料碳排放因子(不含电池)

Table 4	watemai distribution	of neavy-duty	truck venicie	es and mater.	lai carbon en	inssion facto.	is (excluding	batteries)	
项目名称	钢	铸铁	塑料	铸铝	橡胶	玻璃	锻造铝	铜	其他
柴油重卡组成/%	63.37	12.25	8.95	4.95	2.69	2.63	2.19	1.50	1.47
电动重卡组成/%	67.85	2.87	9.46	5.98	2.34	3.35	0.92	4.53	2.70
碳排放因子(以CO ₂ 计)/t·	t ⁻¹ 2.50	0.88	2.40	2.62	2.76	1.62	2.62	2.50	2.24

项目		2021年	STEPS情景		APS	情景	NZE情景	
		2021 平	2030年	2050年	2030年	2050年	2030年	2050年
发电量占比/%	太阳能光伏	3.82	13.25	27.29	14.49	33.93	14.91	34.71
	风能	7.68	13.87	23.11	14.41	27.09	17.40	27.81
	核能	4.78	5.78	8.44	6.56	9.31	7.35	9.52
	天然气	3.41	3.10	2.40	2.89	2.06	4.04	4.62
	煤炭	62.89	47.08	21.76	44.36	9.42	37.85	4.85
	水电	17.41	16.93	16.99	17.30	18.19	18.45	18.50
总发电量/kW·h		8.539 0×10 ¹²	1.113 6×10 ¹³	1.434 2×10 ¹³	1.095 8×10 ¹³	1.610 9×10 ¹³	1.023 2×10 ¹³	1.532 9×10 ¹³

(3)既定政策(STEPS)情景 无新政策出台, 全球能源需求将在2030年前以每年约0.8%的速度 增长,这一增长需求基本由可再生能源满足.

以上情景为国际能源署(IEA)^[39,40,43]对中国设置 的3种电力发展情景,代表了不同的电力结构变化, 反映了不同的电力碳排放因子变化趋势,将其应用 于本研究进行分析可更全面地预测重卡全生命周期 碳排放.

2.2 能源碳排放因子预测

Table 6

600

500

400

300

200

100

2020

2026 2028 2030

2024

电力碳排放因子/g·(kW·h)⁻¹

IEA^[39,40]对全球电力需求进行预测,指明不同情 景下电力需求趋势不同,相同情景下现在到2030年 及2030年到2050年的电力需求增长趋势不同.本研 究以 2021 年和 2030 年各发电方式发电量为基准值, 固定各发电方式年发电量增长率,将基准值与本年 度发电量增加值之和作为下一年度发电量现值,预 测计算下一年度发电量.目标年 n,第 i类发电方式 的发电量如式(17)所示.

$$G_{i,n} = G_{i,2021} \cdot (1 + \alpha_i)^{n-2021}, \quad 2021 \le n \le 2030$$

$$G_{i,n} = G_{i,2030} \cdot (1 + \alpha_i)^{n-2030}, \quad 2030 \le n \le 2050$$
(17)

式中, *G_{i, n}*为目标年*n*, 第*i*类发电方式的发电量; *G_{i, 2021}*为2021年第*i*类发电方式的发电量; *G_{i, 2030}*为2030年第*i*类发电方式的发电量.

将式(17)应用于 IEA 对中国 2030 年及 2050 年 发电量预测中,依次得到了 2021~2030 年及 2030~ 2050 年各发电方式发电量的年增长率,如表 6 所示.

表6 个同情景下各友电力式友电重年增长率预测/%								
Predictions of annual	growth not	o for power	concretion	under verieue	gonoration	mathada b	and on differen	t aconomica /0

米山		2021~2030年		2031~2050年			
尖型	NZE情景	APS情景	STEPS情景	NZE情景	APS情景	STEPS情景	
太阳能光伏	18.68	19.22	18.25	6.42	6.36	5.00	
风能	11.73	10.26	9.99	4.44	5.20	3.89	
核能	7.01	6.48	5.18	3.34	3.73	3.21	
天然气	3.97	0.92	1.91	2.7	0.22	-0.01	
煤炭	-3.57	-1.10	-0.26	-7.95	-5.67	-2.56	
水电	2.69	2.73	2.68	2.03	2.19	1.29	

同理用于 Zhang 等^[11]对柴油机每5 a 下降 3% 碳 排放量的预测,使用 2021 年柴油碳排放因子计算 2026 年柴油碳排放因子,进而通过式(2)可得柴油 碳排放因子年下降率为 0.61%.

将以上发电方式的年增长率与柴油碳排放因子的年下降率代入先前建立的能源排放因子测算模型 [式(1)和式(2)]得到未来柴油碳排放因子及NZE、 APS和STEPS这3种情景下的电力碳排放因子变化 趋势,如图2所示.



2.3 电动重卡与柴油重卡全生命周期碳排放对比

通过式(3)~(6)、式(9)和式(12)计算 NZE、 APS和STEPS情景下两类重卡的全生命周期碳排放,

> 2040 2042

2044 2046 2048 2048



图 2 2021~2050年电力和柴油碳排放因子变化趋势

Fig. 2 Trends in electricity and diesel carbon emission factors from 2021 to 2050

结果如图3所示.

由图3可知,生产阶段和拆解回收阶段两类重 卡碳排放类似,但相比于柴油重卡,电动重卡增 加了电池生产与拆解回收环节产生的碳排放,而 该碳排放却占两阶段碳排放的主导,致使电动重 卡在生产阶段和拆解回收阶段的碳排放远高于柴 油重卡,分别为柴油重卡的2.46倍和28.67~29.35 倍,电池生产和电池回收分别成为生产阶段及拆 解回收阶段碳减排效益不佳的主要原因;图3中两 类重卡生产阶段产生的碳排放不受情景影响是由 于本文参考以往研究,将两类重卡在该阶段产生 的碳排放分摊至各组成材料的生产过程中.运行阶 段,电力和柴油碳排放因子逐年降低使得两类重 卡碳排放均呈逐年下降趋势,其中电动重卡年碳 排放降幅大于柴油重卡是因为电力碳排放因子相 较于柴油碳排放因子下降更快;3种情景下电动重 卡碳排放均从峰值125.63 t开始下降,2027年NZE 情景下降至95.42 t,APS 情景下降至103.05 t, STEPS 情景下降至106.31 t,柴油重卡碳排放则不 受情景影响从256.65 t下降到2026年的248.95 t; 2027年柴油重卡和2028年电动重卡运行碳排放骤 降的主要原因是车辆寿命到期导致该年未能达到 正常的年运行里程.3种情景下两类重卡全生命周 期碳排放由高到低均为运行阶段、生产阶段和拆 解回收阶段,其中运行阶段能源消耗产生的碳排 放皆占全生命周期碳排放的90%以上,为两类重 卡碳排放的主要来源.研究还发现电动重卡碳排放 对电力碳排放因子具有极强的敏感性,电力碳排 放因子(以CO₂计)每降低1g·(kW·h)⁻¹,电动重卡 驶完生命周期行驶里程碳排放可减少1.74 t.





鉴于两类重卡生命周期行驶里程所存在的差 异,将全生命周期碳排放均分至生命周期行驶里程 中,以此获得了单辆电动重卡替代单辆柴油重卡 (单车替代)的每公里碳减排量,进而得到了"单车 替代"的碳减排率,并以电动重卡生命周期行驶里 程为基准评估了"单车替代"产生的全生命周期碳 减排量,结果如图4所示.

从图 4 可以看出,3 种情景下,"单车替代" 均具有较好的减排效益.减排效益由高到低依次 为 NZE 情景、APS 情景和 STEPS 情景,对应的百 公里碳减排量分别为 0.129、0.125 和 0.123 t,全生 命 周 期 碳 减 排 量 分 别 为 1 054.68、1 021.78 和



heavy-duty truck replacing a diesel one

1 007.97 t, 碳减排率分别为 54.38%、 52.68% 和 51.97%.

2.4 模型碳排放结果对比

研究对象差异会直接影响模型的输入参数变 化,进而导致计算结果出现较大偏差.为与相关研 究进行有效对比,保守起见,将模型在STEPS情景 下的碳排放结果与已有模型在相同输入参数下的碳 排放结果进行比较,结果如表7所示,负值表示拆 解回收产生的碳减排量.

由表7可知,本模型与已有模型在各阶段碳排 放趋势一致,从大到小均为运行阶段、生产阶段、 拆解回收阶段,两类重卡在运行阶段碳排放皆占全 生命周期碳排放90%以上,且电池产生的碳排放在 拆解回收阶段中占主导地位.不同模型得到的碳排 放结果各异,这主要是由于模型自身设定的初始值 不同导致,模型2和模型3分别将两类重卡的车辆 生产以固定排放值(以CO2计)8.18 kg·kg⁻¹和8.10 kg·kg⁻¹进行分析,忽略了两类重卡组成结构的差异 以及各组成材料生产加工过程中产生碳排放的不 同,致使两类重卡在车辆生产阶段皆出现了较高的 碳排放结果.本模型充分考虑该点不足,使得车辆 在生产阶段的碳排放计算更为合理.此外,本模型 逐年累计得到的柴油重卡运行阶段碳排放最低,这 与未来能源碳排放因子变化趋势一致,模型1计算 的电动重卡运行阶段碳排放比本模型低,是因为该 模型未考虑线损率、厂用电率以及充电效率对上游 发电量产生的影响.综上所述,与模型1~模型3相 比,本模型对两类重卡全生命周期的碳排放计算更 为精确.//

\sim	/	b	11/	表7 不	同模型碳排放	(结果对比/t	100	V		2)
11	/M	lj .	Table 7	Comparison	of carbon emiss	sions for differe	nt models/t	5	~	50
2	SIL	柴油	重長	SOV	J.		电动	重卡	6	. 5
项目	仕产险段	运行	拆解回收	全生命	车辆生产	电池生产	运行险段	车辆拆解回	电池拆解	全生命
22	王) 例权	阶段	阶段	周期	阶段	阶段	超目的权	收阶段	回收阶段	周期
模型1 ^[11]	23.09	1 663.45	0.76	1 687.30	19.96	4.88	777.85	0.71	22.15	825.56
模型 2 ^[44]	69.53	1 663.45	-11.82	1 721.17	65.60	45.54	912.27	-11.15	-6.06	1 006.20
模型3 ^[45]	68.00	1 663.45	-11.56	1 719.89	64.16	39.76	912.27	-10.91	-7.55	997.73
本模型	19.39	1 635.82	0.46	1 655.67	19.42	28.20	870.55	0.42	12.95	931.54

3 结论

(1)将能源碳排放因子与重卡寿命和生命周期 行驶里程耦合,分阶段构建了电动重卡与柴油重卡 的动态碳排放模型.

(2)电池产生的碳排放在电动重卡生产阶段和 拆解回收阶段中占比分别为59.21%和96.88%,导致 电动重卡在两阶段碳排放分别为柴油重卡的2.46倍 和28.67倍~29.35倍.

(3) "2050年净零排放(NZE)情景"、"承诺目标 (APS)情景"和"既定政策(STEPS)情景"下,两类 重卡运行阶段碳排放皆占全生命周期碳排放90%以 上,该阶段以中间向两端辐射的方式提升了整体碳 减排效益,电力碳排放因子(以CO₂计)每降低 1g•(kW•h)⁻¹,电动重卡全生命周期碳排放可减少 1.74 t. (4)3种情景下,电动重卡均具有较好的碳减排 效益,碳减排效益由高到低依次为NZE情景、APS 情景和STEPS情景,全生命周期碳减排量分别为 1054.68、1021.78和1007.97t,碳减排率分别为 54.38%、52.68%和51.97%.

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