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## 水源水库暴雨径流过程水体锰的迁移及其影响

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摘要:针对西安金盆水库 2017 年汛期出现的锰浓度超标问题,对水库上游至主库区沿程多个监测点垂向锰浓度及其赋存形态进行监测,研究暴雨径流对水中锰含量的影响以及径流中锰的形态,估算单次典型暴雨径流过程水库水体锰的汇入、输出与沉积量,根据实测数据与计算结果,从运行调度角度提出了暴雨时期高浊、高负荷径流入库的规避方案.结果表明,强降雨过程引起的高浊径流汇入显著增加了西安金盆水库水体总锰浓度,导致水库水质严重恶化,2017 年 10 月 12 日至 2017 年 10 月 14 日单次降雨径流总锰的输入负荷为 9.11 t,泄洪和出水输出的总锰为 6.22 t,净沉积量(锰)为 1.47 t.水库上游沿程水体锰含量及形态变化表明,连续降雨过程对土壤的冲刷和侵蚀作用导致大量颗粒态污染物随径流汇入水体,占水体中总锰的质量分数大于 70%,铁锰氧化物结合态为其主要形态.通过与不同粒径范围的颗粒进行相关性分析,颗粒态锰粒径约为 2~20 μm.暴雨径流入库时期采取泄洪排浊的措施可以有效减小锰的污染负荷,降低供水安全风险.

关键词:水源水库; 锰污染; 暴雨径流; 锰形态; 污染负荷; 迁移

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# Migration Characteristics of Manganese During Rainfall Events and Its Impacts on Water Quality in a Drinking Water Source Reservoir

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Abstract: In view of the problem of excessive manganese concentrations in the Xi'an Jinpen Reservoir during the flood season in 2017, the vertical distribution of manganese in density currents and its occurrence pattern were monitored at multiple monitoring sections along the upstream reaches to the main basin. The influences of density currents plunging into the reservoir on the migration and transformation of Mn were studied, and sedimentation, output, and deposition of manganese in the reservoir water were also specifically estimated during a single, typical storm runoff process. Devices for avoiding high turbidity and high load inflows in rainfall events were proposed. The results showed that significant increases of total manganese were induced by high-turbidity inflows, which largely degraded water quality during rainfall events. From 12 to 14 October, 9.11 tons of total manganese were transported into the reservoir during a single rainfall event, and the pollution conditions were largely remitted by flood discharges with an output of 6.22 tons; thus, the net deposition (manganese) was 1.47 tons. The manganese content and morphological changes along the upper reaches of the reservoir indicated that soil erosion occurred during the continuous rainfall process, and this caused a large amount of particulate pollutants to flow into the water body with the runoff. More than 70% of the total manganese in the water was in the iron-manganese oxide bound state. Correlation analysis was conducted with particles of different particle size ranges, and granular manganese particle sizes were about 2-20 µm. The findings indicate that when flood discharges with turbidity currents occur, this can effectively reduce the load of pollutants and the safety risks of water.

Key words: water source reservoir; manganese pollution; storm runoff; manganese form; pollution load; migration

锰元素约占地壳的 0. 1% <sup>[1]</sup>,在天然水体中以溶解态和颗粒态的形式存在 <sup>[2]</sup>.我国Ⅲ类地表水中锰的限值为 0. 1 mg·L <sup>-1[3]</sup>,长期饮用锰含量较高的水可导致人体神经系统和大脑受到损害 <sup>[4]</sup>.同时,高浓度含锰饮用水还存在一系列浊度、色度问题 <sup>[5,6]</sup>,对城市给水厂的处理工艺和设备造成影响,增加给水处理的难度 <sup>[7]</sup>.

湖泊、水库水体锰的来源主要分为沉积物内源 污染释放和外源污染汇入.深层水体周期性热分层 过程极大地阻碍了上下层水体的物质交换<sup>[8]</sup>,底层 水体溶解氧无法得到补充,逐渐出现厌氧状态<sup>[9]</sup>,沉积物在水体厌氧时期较低还原性条件下释放大量还原性污染物,形成内源污染.外源污染则是指通过径流汇入等方式将污染物输送至湖库的过程.强降雨过后,暴雨径流的侵蚀和动态混合作用会导致

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水体颗粒态污染物显著增加<sup>[10,11]</sup>,两岸土壤中的锰会随着降雨径流冲刷汇入水体<sup>[12]</sup>,造成突发性的水体锰污染问题<sup>[13]</sup>,所以暴雨径流输汇就成为了外源污染的主要来源。目前,国内外关于地表径流锰污染的研究多集中在城市地表径流污染以及模型预测分析上<sup>[14~17]</sup>。而对暴雨径流期间水源水库锰的时空变化、锰形态分析以及负荷计算却鲜见报道。水源水库具有水体紊动性差、水力停留时间长等特点,暴雨径流产生的高负荷污染会对水库供水安全产生很大的影响。

本文以西安金盆水库作为研究对象,对 2017 年汛期水库及上游断面水质进行连续监测,分析暴 雨径流期间水体中锰的来源、迁移过程和演变规 律,计算暴雨径流期间锰的污染负荷,以期为水库 在汛期可能出现的锰污染问题提供理论指导和分 析,同时优化水库污染防控管理策略.

#### 1 材料与方法

#### 1.1 研究区域概况

黑河金盆水库位于陕西省西安市周至县黑河峪口以上1500 m处,属于典型的峡谷型水库,流域周边植被覆盖率高,是西安市最主要的饮用水水源地.库区面积 4.55 km²,最大水深 106.00 m,高水位 594.00 m.每年 6~10 月份为金盆水库的防汛期,汛限水位 593.00 m,设计、校核洪水位分别为594.34 m 和 597.18 m.

#### 1.2 采样点布置及分析方法

#### 1.2.1 样品采集及保存

采样点自上游退水线至主库区引水塔设置 S0、S1、S2、S3、S4、S5、S6、S7、S8、S9 和 S10 等多个监测点,S9 代表入库点,S10 代表主库区,其余 10 个点依次代表上游沿程断面,如图 1 所示. 采样监测时间为 2017 年全年,其中 S9 和 S10 的监测频率为每周一次,在暴雨径流时期对上游至库区所有断面进行加密监测. 采样方式:选取水面以下 0.5 m至底部沉积物以上 0.5 m 水体,以 10 m 为间隔使用直立式采样器进行取样. 水样采集完成后使用预酸化的 1.5 L 高密度聚乙烯瓶密封,及时运回并存入 4℃冰箱中,用于锰、悬浮颗粒(SS)等指标的测定.

#### 1.2.2 水体、沉降颗粒中锰的测定

将采集的部分样品经 0.45 μm 孔径滤膜过滤后加浓硝酸酸化,将 pH 调至 2 以下,测得澄清液中的锰含量即为溶解态锰.未过滤的原水样经浓硝酸消解定容后测定的锰为总锰.总锰减溶解态锰为颗粒态锰<sup>[18]</sup>.

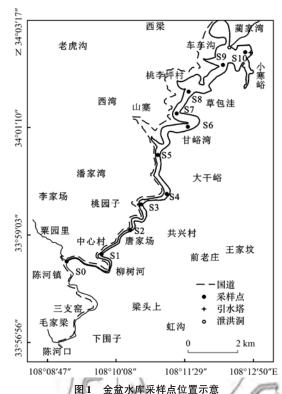


Fig. 1 Sampling sites in the Jinpen Reservoir

为测定水体悬浮物中锰的含量,于10月12~ 26 日, 使用内径 15 cm 的沉降颗粒收集器在主库区 S10 底部收集水体沉降固体颗粒. 悬浮颗粒中锰的 测定方法如下[19]: 称取 0.2(±0.0005)g 干燥的悬 浮颗粒物于50 mL 聚四氟乙烯烧杯中, 加入5 mL 硝酸和1 mL 氢氟酸, 置于电炉上消煮, 蒸发至近 干; 再加入1 mL 硝酸、2 mL 高氯酸和1 mL 氢氟 酸,加热蒸至近干,消解完成后,将溶液和残渣转 移至50 mL 比色管中, 定容, 澄清, 取上清液待测. 悬浮颗粒中锰化学形态分析方法参照 Tessier 等[20] 提出的五步连续提取法进行测定, 依次提取锰的可 交换态、碳酸盐结合态、铁锰氧化物结合态、有机 结合态、残渣态. 消煮液和上清液中的锰采用火焰 原子吸收光谱仪测定, 测定样品时, 除用空白对照 消除误差外增加平行组对照,此次测定的锰回收率 范围在90%~110%,平行样之间的相对标准偏差 小于5%.

水深、浊度、温度等相关理化指标选用美国 HACH Hydro-Lab DS5 多功能水质分析仪进行原位 监测. 经预处理后样品分别使用高碘酸钾氧化光度 法<sup>[21]</sup>和原子吸收光谱仪测定,悬浮颗粒粒径使用 激光粒度分布测定仪测定.

#### 2 结果与讨论

#### 2.1 降雨量分布及流量变化

由图 2 可以看出, 2017 年降雨过程主要集中在

8~10月,各月降雨量分布有较大差异.其中,8月 中上旬整体降雨量较少,8月下旬降雨量有所增 多, 但整体变化幅度较小, 降雨量均小于30.0 mm, 因此并未导致入库流量显著增大. 9月28日起, 出 现几次大规模降雨事件,10月8~11日总降雨量高 达 123.6 mm, 此次强降雨过程使得入库流量由 37.2 m³·s⁻¹急剧增加至404.3 m³·s⁻¹, 为入汛以来 最大值. 总体来看, 2017 年汛期降雨历时较长, 入 库流量随降雨量有同步增长趋势, 但由于地表径流 的形成需要一定时间,故入库流量的变化相对滞后 于地表径流. 水库的日常出库流量在 13~29 m3·s-1, 汛期强降雨导致水库水深急剧增加, 水位 高程由 8 月 1 日的 577. 29 m 升至 10 月 12 日的 594.01 m, 为保证水库正常供水和运行安全, 于10 月4日开始通过泄洪调控水位,出库流量也因此大 幅上升.

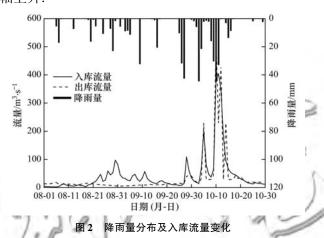


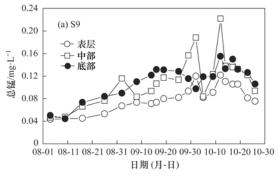
Fig. 2 Distribution of precipitation for in/outflow in 2017

#### 2.2 汛期前后锰随时间的变化

图 3 为 2017 年暴雨径流入库前后 S9 和 S10 水体中总锰浓度的变化,从中可以看出,随高浊暴雨径流汇入,库区水体总锰浓度呈现出逐步增大的趋势.其中 8 月初水体总锰浓度较小,均值为 0.05 mg·L<sup>-1</sup>,且各层水体无明显差异.之后,随水体热分层过程不断加剧,水体底部溶解氧不断

降低(8月17日底部溶解氧降至1.57 mg·L<sup>-1</sup>), 沉积物向上覆水体释放少量铁锰等还原性污染 物:同时伴随着降雨过程,入库流量增大,径流中 携带的锰使得底部和中部水体锰浓度明显增加. 9 月14日S10水体中部和底部锰浓度最大值已达到 0.158 mg·L<sup>-1</sup>, 针对这一情况, 金盆水库开启扬 水曝气系统, 在混合充氧过程中, 水体溶解氧浓 度增大,其氧化还原环境逐步由还原态向氧化态 转变,抑制了沉积物中锰的释放;同时较高浓度 的溶解氧加速水体中溶解态锰氧化、沉积[22]. 运 行至9月29日,水体锰浓度最大值由0.223 mg·L<sup>-1</sup>削减至 0.143 mg·L<sup>-1</sup>.9 月 28 日和 10 月 11 日平均入库流量达到 108.9 m<sup>3</sup>·s<sup>-1</sup>和 404.3 m3·s-1,暴雨径流形成含锰污染物对水库锰浓度 影响较大,潜流作用使中部水体锰变化最为剧烈, 其中10月12日S9和S10中部水体锰浓度已达到 0. 222 mg·L<sup>-1</sup>和 0. 198 mg·L<sup>-1</sup>. S9 相比 S10 受径 流影响更为显著,一方面颗粒态锰沿程沉降,另 一方面水库汛期泄洪时, 中部水体部分高浓度的 锰自入库点 S9 进入主库区 S10 过程中从泄洪塔排 出,S10 锰浓度会相应减小.10 月12 日之后,入 流量减小, 径流给水库带来的外源污染逐渐消失 至10月26日, 主库区总锰浓度已降低至0.084  $\operatorname{mg} \cdot \operatorname{L}^{-1}$ .

暴雨径流导致水体锰污染主要是由于降雨形成的地表径流对土壤产生强烈的冲刷和侵蚀,径流携带锰污染物由上游河道进入水库,对库区水质造成影响<sup>[23]</sup>.杨帆等<sup>[24]</sup>的研究发现,西湖龙泓涧流域在发生降雨事件时,径流中污染物的平均浓度与降雨量、降雨历时、降雨强度有较好的相关性,且污染物迁移通量随降雨量的增大而增大.陈心凤等<sup>[25]</sup>发现舟山水库铁锰超标集中在汛期,暴雨径流冲刷土壤,由于酸性降雨的淋溶作用,土壤中释放出的可溶态锰将随着地表径流一同汇入水体,对河流和水库造成污染.



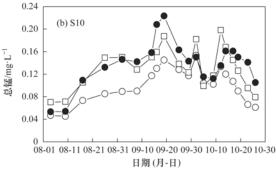


图 3 径流前后水体总锰浓度变化

Fig. 3 Changes of total manganese concentrations during rainfall events

#### 2.3 暴雨径流期间锰负荷计算

#### 2.3.1 输入负荷

为评估暴雨径流对水库水体锰的输送过程,针对 10 月 12~14 日单次较大暴雨径流,计算暴雨径流,过程中锰的输入负荷.

根据金盆水库提供的库情资料以及入库点 S9 断面水体总锰平均浓度,采用如下公式<sup>[26]</sup>计算锰的输入负荷:

$$I = K \times \sum_{i=1}^{n} Q_{i} \times c_{i}$$
 (1)

式中, I 为暴雨径流期间主库区锰的输入负荷, t; K 为计算时段的时间转换系数, 0.0864;  $Q_j$  为第 j 日平均入库流量,  $m^3 \cdot s^{-1}$ ;  $c_j$  为 S9 取样点第 j 日水体锰平均浓度,  $mg \cdot L^{-1}$ .

经计算,3 d 内锰的输入负荷为 9.11 t. 仅 10 月 12 日,暴雨径流输入主库区的锰负荷就达到 5.80 t,占总输入负荷的 63.7%,所以暴雨径流会产生极大的输入负荷.

#### 2.3.2 输出负荷

本研究同时计算了此次暴雨径流期间锰的输出 负荷,这一期间水体含锰污染物主要以水库饮水塔 出水、汛期泄洪以及沉积这3种主要形式离开 水体.

#### (1)出水及泄洪

水库供水产生的输出负荷计算方法与上述输入 负荷的计算方法类似. 出水的锰浓度采用引水洞 (高程 554 m)所处水层的平均锰浓度计算. 而泄洪 产生的输出负荷由泄洪当天泄洪洞流量和泄洪洞 (高程 545 m)所处水层的平均锰浓度计算,按公式 (2)计算:

$$Z = K \times \sum_{j=1}^{n} Q'_{j} \times c'_{j} + K \times \sum Q' \times c' \quad (2)$$

式中, Z 为出水及泄洪产生的输出负荷, t; K 为计算时段的时间转换系数, 0. 086 4; Q' 为第 j 日平均

出库流量,  $\mathbf{m}^3 \cdot \mathbf{s}^{-1}$ ;  $c_j'$  为第 j 日引水洞所处水层锰平均浓度,  $\mathbf{mg} \cdot \mathbf{L}^{-1}$ ; Q'为泄洪当天泄洪洞的平均出流量,  $\mathbf{m}^3 \cdot \mathbf{s}^{-1}$ ; c'为泄洪洞所处水层水体的平均锰浓度,  $\mathbf{mg} \cdot \mathbf{L}^{-1}$ .

经计算,水库供水产生的锰输出负荷为 1.36 t,由 10 月 12 日和 10 月 14 日泄洪产生的锰的输出负荷为 4.86 t,可以看出泄洪在一定程度上削弱暴雨径流过程中锰的大量输入对于水库水质的影响.

#### (2) 沉积量

汛期输入的锰主要是颗粒态锰,相比于其他时期,暴雨径流时期锰的沉积量较大.根据式(3)计算锰的沉积量:

$$V = I - Z - \Delta M \tag{3}$$

式中,V为沉积量,t;I为暴雨径流时期锰的输入 负荷,t;Z为出水及泄洪产生的输出负荷,t; $\Delta M$ 为计算时段前后水体中锰含量的变化t.

径流前后水体中锰含量的变化由金盆水库提供的水深-库容资料和对应水层的锰平均浓度计算. 本研究中自水体表层以下 0.5 m 至底部以上 0.5 m 为区间,以 10 m 为间隔将水体垂向划分 9 层,按式(4)计算:

$$\Delta M = \sum c_1 \times V_1 - \sum c_b \times V_b \tag{4}$$

式中, $\Delta M$  为计算时段前后水体中锰含量的变化,t;  $c_b$  为 10 月 12 日前各水层总锰平均浓度, $mg \cdot L^{-1}$ ;  $V_b$  为各水层体积, $m^3$ ;  $c_l$  为 10 月 14 日后各水层总锰平均浓度, $mg \cdot L^{-1}$ ;  $V_l$  为各水层体积, $m^3$ .

水体中锰在暴雨径流前后含量变化  $\Delta M = 1.42$  > 0, 锰的沉积量为 1.47 t, 大量颗粒态锰富集在表层沉积物上, 沉积物污染加剧 [27], 增加了水体底部内源污染物释放的风险.

此次暴雨径流过程中锰的输入、输出负荷等计算结果汇总于表1中.

表1 暴雨径流过程中水体锰的负荷计算/t

Table 1 Load calculations for manganese in the water body during storm runoff/t

日期(月-日)	输入负荷	出水负荷	泄洪负荷	水体锰含量变化	沉积量
10-12	5. 80	0.48	3. 86	_	_
10-13	2. 26	0. 45	_	_	_
10-14	1. 05	0.43	1.00	_	_
总计	9. 11	1. 36	4. 86	1. 42	1. 47

#### 2.4 暴雨径流过程中水体锰的组成

#### 2.4.1 水体中锰的赋存形态

10月12日大径流入库时,自上游S2断面至主库区S10断面水体中锰的赋存形态的变化结果如图4所示. 受暴雨径流影响,各个断面上水体锰形态

均以颗粒态为主. 其中, S2、S3 和 S4 断面所处的上游河道窄、水深浅,整个断面受径流汇入的影响均较大,且酸性降雨的冲刷会使土壤中离子代换作用增强而加速金属离子淋溶释放<sup>[28]</sup>,所以这 3 个断面上溶解态锰占总锰的比例高于其他断面,所占

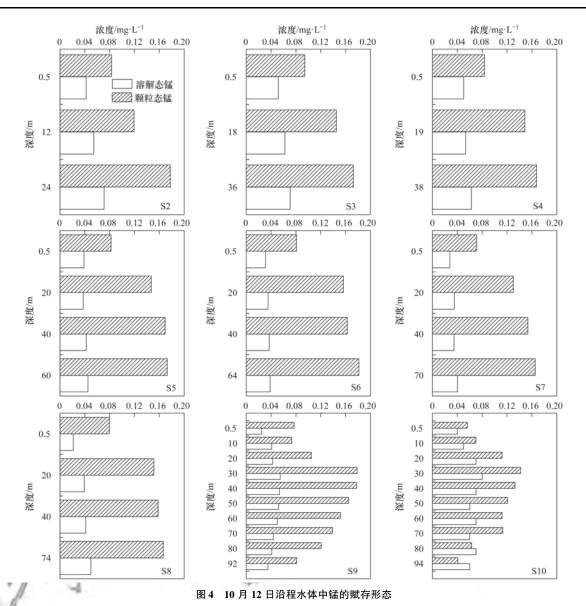


Fig. 4 Occurrence of manganese in waters along the river on October 12

百分比分别为 30.63%、30.97% 和 29.34%.从 S5 断面开始由于水深急剧增大,稀释作用等因素,溶解态锰所占的比例降低, S5~S8 断面溶解态锰所占比例分别是 22.25%、19.63%、20.97% 和 20.05%.径流自 S9 断面以潜流的方式进入主库区后,水体流动性减弱,加之悬浮颗粒的沉降等作用,颗粒态锰的比例迅速降低,溶解态锰占比由 S8 断面处的 20.05%增加至 S9 断面的 25.72%和 S10 断面的 39.55%.

曾康等<sup>[29]</sup>的研究表明,在暴雨径流期间,金盆水库中部水体的氮磷等营养盐变化显著,主要是因为颗粒态污染物随异重流潜流进入水体.本研究中锰的垂向变化也有相同的趋势,上游 S2~S8 各个断面水体垂向颗粒态锰浓度逐渐增加,以 S2 断面为例,表层和中部水体颗粒态锰浓度分别为 0.083 mg·L<sup>-1</sup>和 0.119 mg·L<sup>-1</sup>,而底部颗粒态锰浓度达到最大值 0.178 mg·L<sup>-1</sup>.随着潜流过程中较大粒径

的颗粒物沉降,水体中颗粒态锰沿程逐渐减少,至主库区 S10 断面,颗粒态锰浓度最大值降低至0.142 mg·L<sup>-1</sup>,占总锰比例为64.96%,该峰值位于中部水层30 m的位置.10月12日为径流形成的初期,异重流为水体中部潜流,整个垂向表现为中部大,上部和底部低,表明此次水体中的锰是以颗粒态锰为主要赋存形态.

#### 2.4.2 颗粒态锰与粒径的关系

粒径是表征颗粒行为的重要参数. 其分布影响着颗粒物的性质与特征,而且与颗粒可迁移性以及污染物浓度有着密切的关系<sup>[30]</sup>. 对 10 月 12 日采集的上游 S2 断面至主库区 S10 断面不同深度的水样中悬浮颗粒的粒径进行分析,本研究将颗粒粒径分为 3 个部分: <2 μm(黏粒)、2 ~ 20 μm(粉砂)、>20 μm(砂粒). 结果如图 5 所示,上游 S2 ~ S8 断面,水中悬浮颗粒沿程逐渐沉降,其中大颗粒沉降速度较快,所以粒径大于 20 μm 颗粒物的体积分数

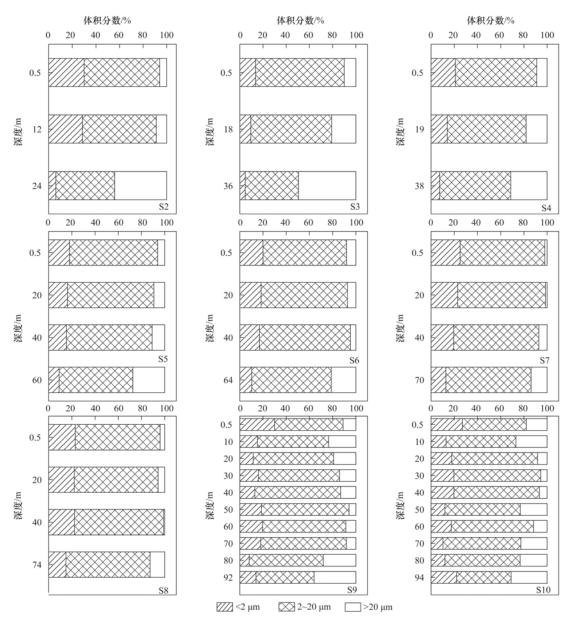


图 5 10 月 12 日沿程水体悬浮颗粒粒径分布

Fig. 5 Distribution of suspended particle sizes in water on October 12

在沿程各断面上也显著减小,最大值由 S2 断面底部 44.08%减小至 S8 断面底部 12.44%. 而粒径小于 2 μm 和 2~20 μm 的颗粒所占体积分数有所增大. 总体来看,2~20 μm 颗粒所占体积分数最大,垂向变化呈现出上游断面随着水深的增大,小于 2 μm 和 2~20 μm 的颗粒体积分数减小,大于 20 μm 的颗粒体积分数逐渐增大的趋势. 自 S9 断面开始由于水深突然增大,发生中部潜流,S9 和 S10 断面处 2~20 μm 颗粒体积分数在水深 20~60 m 之间有明显的突峰.

有研究表明,不同粒径的污染物分布不同<sup>[31]</sup>,为明确悬浮颗粒粒径和颗粒态锰之间的关系,对10月12日S9和S10两个断面颗粒粒径和颗粒态锰浓度进行了Pearson相关性分析,结果列于表2中.水

体中颗粒态锰与 2~20 μm 粒径范围的颗粒在 0.01 水平上呈显著正相关,而与大于 20 μm 粒径范围的颗粒在 0.05 水平上呈显著负相关. 表明随着粒径的增大,颗粒物对锰的吸附能力逐渐减小,颗粒态锰的含量逐渐减小,此次径流汇入的颗粒态锰主要以粒径 2~20 μm 的悬浮颗粒作为载体. 因此,控制暴雨径流输入的颗粒态锰主要是去除粒径较小的粉砂. 金盆水库泄洪洞高程为 545 m, 刚好位于水深 50 m 处,中部水体中粒径范围在 2~20 μm 的颗粒物体积占比大于 70%,所以适时地泄洪是削减水体中锰负荷的有效手段.

#### 2.4.3 颗粒态锰的化学形态

水体中颗粒态锰的赋存形态,可以提供水体污染物存在方式、迁移转化、生化有效性等方面的信

息,是评价锰对水体污染程度及潜在生态危害的重要因素<sup>[32]</sup>.可交换态一般吸附于固体颗粒上,最容易释放;碳酸盐结合态对 pH 值变化敏感;铁锰氧化物结合态在厌氧条件下不稳定易释放;有机结合态可能会因有机质降解而释放;残渣态存在于原生矿物的晶格内,一般不会释放.由图 6 可以看出,此次暴雨径流输入的颗粒态锰的主导形态为铁锰氧化物结合态,各种形态的颗粒态锰所占质量分数依次为:铁锰氧化物结合态(44.01%)>残渣态(26.39%)>碳酸盐结合态(14.03%)>可交换态(11.43%)>有机结合态(4.14%).

#### 表 2 主库区颗粒粒径与颗粒态锰的相关性分析1)

Table 2 Correlation analysis between the particle size and

granulai manganese	in the main re	escryon area	
项目	<2 μm	2 ~ 20 μm	>20 µm
S9 颗粒态锰浓度	-0.123	0. 929 **	- 0. 704 *
S10 颗粒态锰浓度	-0.320	0. 890 **	- 0. 709 *

1) \*表示在 0.05 水平(双侧)显著相关; \*\*表示在 0.01 水平(双侧)显著相关

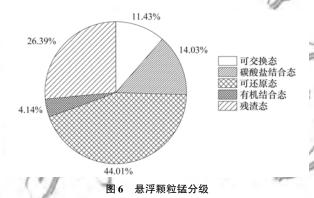


Fig. 6 Manganese classification of suspended particles

此次暴雨径流输入的颗粒态锰以铁锰氧化物结合态为主要迁移形态.根据这5种形态的锰在水体中释放的难易程度,将其划分为3类,其中可交换态和碳酸盐结合态称作易释放态<sup>[33]</sup>、铁锰氧化物结合态和有机结合态称作潜在释放态、残渣态称为非释放态.悬浮颗粒中潜在释放态和非释放态所占比重为74.54%,表明径流冲刷土壤以及颗粒态锰随径流自上游潜入主库区的过程中发生了溶解与解吸现象<sup>[34]</sup>.大量潜在释放态和非释放态的锰进入水体,会随着悬浮颗粒的沉降落入底部沉积物,潜在释放态的锰可能会因为水体底部理化环境(DO、pH、温度等)发生变化而再次释放,对水质造成二次污染.

#### 3 结论

(1)在汛期,强降雨冲刷使得大量污染物随暴 雨径流潜入,导致水体锰浓度急剧增大,主库区总 锰平均浓度最大值达到  $0.152 \text{ mg} \cdot \text{L}^{-1}$ , 水质迅速恶化.

- (2)10月12~14日,总锰输入负荷为9.11 t, 泄洪和出水产生的输出负荷分别为4.86 t和1.36 t.及时采取泄洪除浊措施可有效地减轻暴雨径流 时期锰的污染负荷.
- (3)随径流汇入水体的锰以颗粒态为主要赋存形态.上游至主库区水体中颗粒态锰浓度随着颗粒物沉降逐渐减小.进入主库区后,异重流潜入至水深20~60 m的位置,中部水体中锰浓度显著增加.颗粒态锰中铁锰氧化物结合态所占质量分数高达44.01%,大量潜在释放态的锰沉积增加了内源污染释放的风险.
- (4)水体中悬浮颗粒粒径分布差异明显, 2~20 μm 粒径范围的颗粒所占体积分数与颗粒态锰浓度呈显著正相关, 说明粒径 2~20 μm 颗粒对锰的结合、吸附更为明显.

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