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## 反复冻融与高温老化对砷污染土壤固化稳定化效果的 影响

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摘要:通过无侧限抗压强度、渗透系数、浸出浓度以及形态分布测试,分别考察了不同条件下反复冻融和高温老化作用对砷污染土壤固化或稳定化效果的影响,同时利用扫描电镜分析了稳定化土壤的微观形貌变化.结果表明,反复冻融和高温老化处理均会不同程度地削弱固化土壤的抗压强度,并提高其渗透系数.两种处理会增加稳定化土壤中砷的不稳定形态,从而增大其浸出浓度,如反复冻融处理 300 次后,稳定化土壤中砷的不稳定形态增加了 19.81%,浸出浓度由 115.5 μg·L⁻¹增加至 151.5 μg·L⁻¹,80℃高温老化 10 h 后,砷的不稳定形态增加了 25.1%,浸出浓度增加至 164.5 μg·L⁻¹. 反复冻融次数的增加、老化温度的升高以及老化时间的延长,均会分别增大对固化/稳定化效果的影响.稳定化土壤经反复冻融和高温老化处理后,会发生不同程度的碎裂,呈现结构松散状.

关键词:高温老化; 反复冻融; 砷; 污染土壤; 固化/稳定化

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# Effects of Repeated Freezing and Thawing and High Temperature Aging on the Solidification and Stabilization of Arsenic Contaminated Soil

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Abstract: The impact of solidification and stabilization effects on arsenic (As) contaminated soil before and after repeated freezing and thawing or high temperature aging was investigated by tests of unconfined compressive strength (UCS), permeability, leaching concentration and fractionation. The microstructure appearance of the soil was observed using SEM. The results show that the UCS of solidified soil decreases and its permeability increases after repeated freezing and thawing or high temperature aging. In stabilized soil, the unstable species of As increase and the leaching concentration of As rises accordingly after both treatments. The concentration of unstable species of As increased accordingly by 19.81% and 25.1%, and the leaching concentration rose from 115.5  $\mu$ g·L<sup>-1</sup> to 151.5  $\mu$ g·L<sup>-1</sup> and 164.5  $\mu$ g·L<sup>-1</sup> respectively after 300 freeze-thaw treatments or under 10 h of high temperature aging under 80°C. In general, the influence of the effects increases with more freeze-thaw events and higher temperature aging of longer duration. More damage and fragmentation was observed after both treatments.

Key words: high temperature aging; repeated freezing and thawing; arsenic; contaminated soil; solidification and stabilization

含砷矿石的开采以及砷剂在工业生产中的广泛应用导致了我国土壤砷污染形势十分严峻,包括广西、湖南、广东、新疆在内的诸多省份的土壤都受到了大量的砷污染<sup>[1,2]</sup>.目前,针对包括砷在内的重金属污染土壤,我国应用最为广泛的修复技术是固化/稳定化.该技术是通过物理塑封或改变化学形态降低污染物的迁移能力和生物有效性<sup>[3,4]</sup>,并未从总量上将污染物从土壤中去除,因此对于该技术处理后土壤的稳定性评估方法的选择尤为关键.目前,针对固化/稳定化土壤,我国应用最为广泛的效果评估方法为 硫酸硝酸法<sup>[5]</sup>和醋酸缓冲液法<sup>[6]</sup>.然而,该两种方法均为静态式的土壤重金属浸出方法,无法反映土壤暴露在不同实际场景中的动态变化过程,因此无法有效评估固化稳定化土壤的长期

稳定效果<sup>[7,8]</sup>.事实上,固化/稳定化修复后的土壤在现实应用场景中往往会受到冻融、高温、碳化等自然条件变化的胁迫影响,从而影响其理化性能和长期稳定性能,导致重金属重新释放到自然环境中<sup>[9~11]</sup>.因此,在固化/稳定化效果评估工作中,根据我国地理和气候特征,开展环境胁迫模拟实验,以加速土壤理化性能的变化以及重金属污染物在土壤中的释放,可以为固化/稳定化土壤的长期稳定效果评估提供一定的参考.

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本实验针对重金属砷,通过反复冻融和高温老化处理对固化/稳定化处理前后的污染土壤开展环境胁迫模拟实验,考察不同冻融和高温条件对固化土壤物理性能和稳定化土壤浸出浓度的影响,采用形态分析和扫描电镜等手段对影响机制进行探讨,以期为重金属污染土壤固化/稳定化长期效果评估方法的建立提供数据参考.

#### 1 材料与方法

#### 1.1 供试样品和材料

实验用土壤取自广西某场地,采集 0~20 cm 污染土壤,土壤样品经风干、研磨、过 2 mm 筛后备用.供试土壤 pH 值为 7.2,重金属含量及浸出浓度如表 1 所示.实验用固化剂为普通硅酸盐水泥(A.0 42.5),稳定剂为某商业化稳定药剂,该稳定剂主要成分为天然矿物,已在我国部分重金属污染土壤固化/稳定化修复工程中得到应用.

表 1 供试土壤重金属含量及浸出浓度

Table 1 Total volume and leaching concentration of metals in the soil

重金属	污染含量/mg·kg <sup>-1</sup>	浸出浓度/mg·L <sup>-1</sup>
砷	3141. 67	1.63
镉	0. 24	ND ND
铬	43. 32	ND/
铅	8. 97	ND
锌	40. 57	ND
铜	15. 93	ND ND
镍	14. 83	ND /
汞	0. 22	ND

#### 1.2 实验方法

#### 1.2.1 固化/稳定化处理

取若干供试土壤于搅拌锅中,以35%的添加比例(质量分数)添加水泥,以水土比0.5加入去离子水,于水泥胶砂搅拌机中机械搅拌均匀. 搅拌后的固化土壤分别置于边长为70 mm的立方体试模或内径60 mm,高150 mm的圆柱体试模中制备固化块,静置1 d 后拆模、养护.

取若干供试土壤于玻璃杯中,按实验所用商业稳定剂的一般使用方法以1%(质量分数)添加稳定剂,以水土比1:1添加去离子水,搅拌均匀.

上述固化块与稳定化土壤置于恒温恒湿养护箱 中在相对湿度 95%、温度 20℃条件下养护 7 d.

#### 1.2.2 反复冻融实验方法

取养护完毕的固化或稳定化样品,置于反复冻融箱中(TDR-28,天津港源试验仪器厂)开展反复冻融实验,冻融温度为-20℃~20℃,单次冻融循环

周期约为 3 h, 分别冻融 100、150、200、250 和 300 次.

#### 1.2.3 高温老化实验方法

取养护完毕的固化或稳定化样品,分别在 60℃ 和 80℃下开展高温老化实验,老化时间分别为 4、6、8 和 10 h.

上述实验结束后,固化样品开展无侧限抗压强 度和渗透系数测试,稳定化样品开展浸出浓度测试, 每组实验设置3个平行样品.

#### 1.3 测试分析方法

#### 1.3.1 物理性能测试

采用全自动抗折抗压一体机(DYE-300S,天津港源试验仪器厂)开展无侧限抗压强度测试,采用三轴渗透试验仪(TK-STTP-1,上海深尔科科技有限公司)进行渗透系数测试,即根据一定时间内渗流管中的水在一定固结压力和水压下下降的高度,利用达西定律计算渗透系数.

#### 1.3.2 浸出浓度测试

采用硫酸硝酸法<sup>[5]</sup> 开展浸出浓度测试. 用 pH = 3. 20 ± 0. 05 的硫酸硝酸溶液对土壤样品进行浸提,固液比(质量体积比)为 1: 10,在 30  $\mathbf{r} \cdot \mathbf{min}^{-1}$ 下翻转振荡 18 ~ 20 h.

#### 1.3.3 形态分布测试与土壤形貌观察

采用 Tessier 五步分析方法<sup>[12]</sup>测定砷的形态分布,如表 2 所示. 采用扫描电子显微镜(S-4800,目立)对土壤样品微观结构进行观察.

#### 1.3.4 砷测试方法

采用电感耦合等离子体发射光谱仪(ps7800,日立)对浸出液中的砷进行浓度测定.

表 2 形态分布测试提取方法

Table 2 Fractionation methods

重金属形态	提取条件
离子交换态	1 mol·L <sup>-1</sup> Mg(NO <sub>3</sub> ) <sub>2</sub> (pH 7.0)
碳酸盐结合态	1 mol·L <sup>-1</sup> NH <sub>4</sub> Ac (pH 5.0)
铁锰氧化结合态	0.04 mol·L <sup>-1</sup> NH <sub>2</sub> OH·HCl(pH 2.0)
硫化物及有机结合态	$30\%~\mathrm{H_2O_2}$ ; 0. 02 mol·L $^{-1}~\mathrm{HNO_3}$
残渣态	浓硝酸和高氯酸

#### 2 结果与讨论

2.1 反复冻融对固化/稳定化土壤稳定性能的影响 图 1 显示了不同条件反复冻融处理对固化土壤

物理性能的影响. 污染土壤经水泥固化后,其抗压强度为 3.22 MPa,渗透系数为 1.2×10<sup>-4</sup> cm·s<sup>-1</sup>. 固化污染土壤经 150 次反复冻融后,其抗压强度略有上升,达到 3.88 MPa. 事实上,水泥在污染土壤固

化中,可以通过水化反应形成水合硅酸钙(CSH)以及氢氧化钙等物质,使处理后的土壤具有一定的强度<sup>[13]</sup>. 而 Glasser<sup>[14]</sup>的研究认为,水泥在固化过程中,有三分之二的水化反应是在 28 d 完成. 因此,在冻融 150 次期间,固化土壤内部可能仍在发生水泥水化反应,从而导致抗压强度上升. 而固化土壤反复冻融 200、250 和 300 次后,其抗压强度又降至3.59、3.16 和 3.19 MPa,说明冻融处理对于固化土壤的强度具有一定的削弱影响. 同时,有研究者<sup>[15]</sup>通过压汞实验对冻融前后的固化土壤进行孔隙测定,结果表明冻融处理会增大固化土壤的孔隙体积,从而提高土壤的渗透性能. 本实验中,固化土壤经反复冻融 100、150、200、250 和 300 次后,其渗透系数明显增大,分别为 3.16 × 10<sup>-4</sup>、4.07 × 10<sup>-4</sup>、4.15 × 10<sup>-4</sup>、3.65 × 10<sup>-4</sup>和 3.25 × 10<sup>-4</sup> cm·s<sup>-1</sup>.

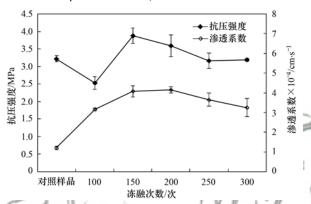


图 1 反复冻融对固化土壤抗压强度及渗透系数的影响 Fig. 1 Unconfined compressive strength and permeability of solidified soil before and after freeze-thaw treatment

由图 2 可知,经稳定化处理后,污染土壤中砷的浸出浓度由1 630 μg·L<sup>-1</sup>降低至115.5 μg·L<sup>-1</sup>,稳定化效果十分显著. 而经过不同次数的反复冻融处理后,稳定化土壤中砷的浸出浓度有所增大,分别为131.5、132.5、139、134.3 和 151.5 μg·L<sup>-1</sup>. 当冻融次数达到 300 次时,砷的浸出浓度增大了31.2%. 这一结果表明,反复冻融处理可能会通过降低土壤对重金属的固持能力,增加土壤中重金属的生态风险<sup>[16]</sup>.

事实上,固化/稳定化处理后的土壤在部分实际 处置方式下,如路基材料等,会因地域不同而受到不 同程度的反复冻融影响. 在短时间内开展多次反复 冻融处理,加速影响固化/稳定化土壤的物理特性和 浸出浓度,在一定程度上可以反映其长期稳定性.

2.2 高温老化对固化/稳定化土壤稳定性能的影响 图 3 显示了不同条件高温老化处理对固化土壤

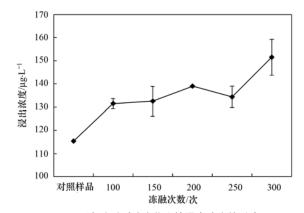


图 2 反复冻融对稳定化土壤浸出浓度的影响

Fig. 2 Leaching concentration of stabilized soil before and after freeze-thaw treatment

物理性能的影响. 从中可知,高温老化处理会削弱固化土壤的抗压强度,在老化温度为60℃时,固化土壤的抗压强度在不同老化时间下由3.22 MPa分别下降至1.89、1.56、1.47 和1.44 MPa. 老化温度提升至80℃时,其对固化土壤抗压强度的影响更大. 同时,80℃高温老化条件下,固化土壤的渗透系数有所升高,但老化温度为60℃时,其对固化土壤的渗透系数影响并不显著.

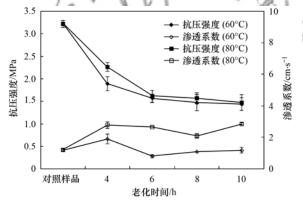


图 3 高温老化对固化土壤抗压强度及渗透系数的影响 Fig. 3 Unconfined compressive strength and permeability of solidified soil before and after high temperature aging

由图 4 所示,60℃老化条件下,高温对稳定化土壤中砷浸出浓度的提升影响并不明显,但当老化温度为 80℃时,砷的浸出浓度在不同老化时间下由 115.5 μg·L⁻¹分别增加至 122.5、150、151 和 164.5 μg·L⁻¹. 事实上,温度是影响重金属淋溶的重要因素之一[17]. 尚小娟等[18]在对垃圾堆肥土壤的研究中表明,温度对重金属的浸出行为表现显著的促进作用. 固化/稳定化土壤在其实际处置场景中,可能会受到局部区域持续高温的影响,采用高温老化胁迫实验加速破坏其稳定性能,在一定程度上可以反映其在实际场景中的长期效果.

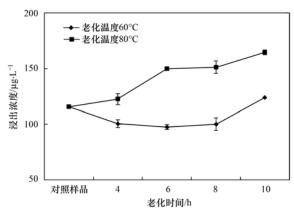


图 4 高温老化对稳定化土壤浸出浓度的影响

Fig. 4 Leaching concentration of stabilized soil before and after high temperature aging

#### 2.3 稳定化土壤中砷的形态分布变化

土壤中砷通常与铁锰氧化物、氢氧化物、碳酸盐和碳酸盐矿物结合[19]. 图 5 反映了稳定化土壤经不同条件反复冻融处理后砷的形态分布变化. 稳定化土壤经过反复冻融处理 100 次后, 砷的形态分布变化不大, 当反复冻融处理 300 次后, 砷的离子交换态、碳酸盐结合态和铁锰氧化结合态分别增加了12.69%、3.06%和4.06%, 硫化物及有机结合态减少了2.46%, 残渣态减少了17.34%. 由此可见, 随着反复冻融次数的增加, 稳定化土壤样品中砷的不稳定形态[20,21]增加, 导致其浸出浓度增大. 有研究者提出[22], 冻融作用可改变土壤水分的分布, 增强土壤释水性能, 促进重金属赋存形态的转化.

由图 6 所示,高温老化处理中的温度越高,对主壤中砷的形态分布影响越大. 如 60℃老化 4 h 和 10 h 后, 砷 的 不稳定形态由 48.2% 分别增加至51.32%和53.15%,而经80℃老化 4 h 和 10 h 后, 砷的不稳定形态发生了明显的提升,分别为71.47%和73.33%.而在相同老化温度下,随着老

化时间的延长,不稳定形态有所增加.这一形态分布的变化趋势与上述浸出浓度变化趋势保持一致.

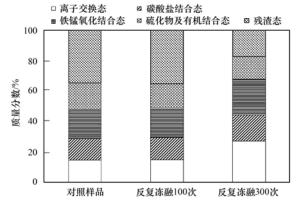


图 5 反复冻融对稳定化土壤中砷的形态分布影响

Fig. 5 Fractionation of As in stabilized soil before and after freeze-thaw treatment

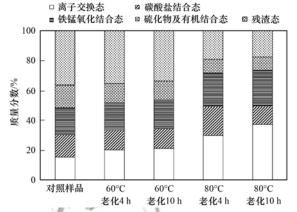
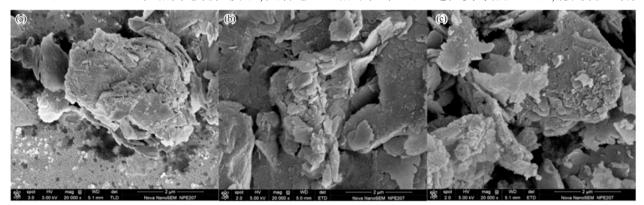


图 6 高温老化对稳定化土壤中砷的形态分布影响

Fig. 6 Fractionation of As in stabilized soil before and after high temperature aging

#### 2.4 土壤形貌及结构变化

图 7 反映了稳定化土壤经不同条件反复冻融处理后的微观形貌变化. 从中可知,对照稳定化样品相对致密. 而经过反复冻融处理后,稳定化土壤发



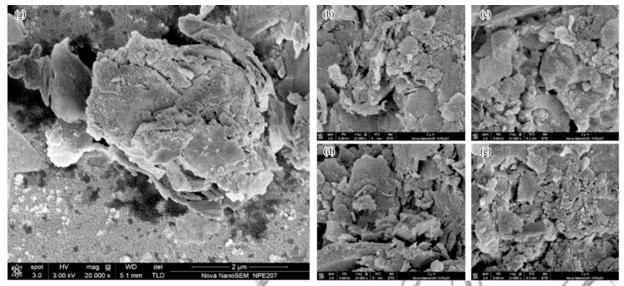
(a) 对照样品; (b) 反复冻融 100 次; (c) 反复冻融 300 次

图 7 不同反复冻融循环次数的土壤样品扫描电镜结果(×20000)

Fig. 7 SEM images of soils before and after freeze-thaw treatment (  $\times 20000$ )

生不同程度的碎裂,结构松散,呈现较多碎散晶体,这一现象与丛鑫等<sup>[23]</sup>的研究结果类似.同时,土壤冻结时,孔隙中冰晶的膨胀作用会打破颗粒与颗粒之间的联结,融化时会将土壤大团聚体破碎成小团聚体<sup>[24,25]</sup>.由图 8 所示,高温老化处理同样会影响

稳定化土壤的微观结构,随着老化温度升高、老化时间延长,土壤的破碎程度越大.相对于反复冻融处理,高温老化对土壤微观结构的破碎影响更大,这可能是由于高温处理过程中土壤含水率急剧下降所致.



(a)对照样品; (b)60℃老化4 h; (c)60℃老化10 h; (d)80℃老化4 h; (d)80℃老化10 h

图 8 不同老化阶段土壤样品的扫描电镜结果(×20000)

Fig. 8 SEM images of stabilized soils before and after high temperature aging ( ×20 000)

#### 3 结论

- (1)反复冻融或高温老化处理会在一定程度上削弱固化土壤的抗压强度并提高其渗透系数.同时,两种处理会增加稳定化土壤中砷的浸出浓度.冻融次数的增加或老化温度和老化时间的升高,会加大对固化/稳定化土壤稳定性能的破坏.
- (2)稳定化土壤经过反复冻融或高温老化处理 以后,其砷的不稳定形态均有所增加,土壤呈现结构 松散状,并产生较多碎散晶体和结构缝隙.
- (3)在固化/稳定化土壤的效果评估中,增加反复冻融或高温老化等环境胁迫模拟实验,以加速土壤理化性能的变化以及重金属污染物在土壤中的释放,可以在一定程度上反映固化/稳定化土壤的长期稳定效果.

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